

Docket No. MIT8003L

Box Patent Application
Assistant Commissioner of Patents
Washington, D.C. 20231

NEW APPLICATION TRANSMITTAL

Transmitted herewith for filing is the patent application of :

Inventor(s): Guy W. Carlisle

For (title): IMAGING SYSTEM WITH A TWO-AXIS-GIMBAL
MIRROR SCAN SYSTEM APPARATUS AND METHOD

1. Type of Application

- ☒ Utility
☐ Design

2. Benefit of Prior U.S. Application(s) Under 35 U.S.C. §120

This application is a:

- ☐ Divisional
☐ Continuation
☐ Continuing Patent Application (CPA)
☐ Continuation-in-part (CIP),

and hereby claims benefit under 35 U.S.C. §120 to the following applications:

| SERIAL NUMBER | FILING DATE |
|---------------|-------------|
| None | |

3. Benefit of Non-U.S. Application Under 35 U.S.C. §119(a)-(d)

This application claims priority under 35 U.S.C. §119(a)-(d) to the following foreign application(s) and/or inventor certificate(s):

| COUNTRY | APPLN. NUMBER | FILING DATE |
|---------|---------------|-------------|
| None | | |

Certified copy(ies) of the application(s) and/or inventor certificate's from which priority is claimed:

- ☐ is(are) attached;
☐ will follow.

4. Benefit of Provisional Application Under 35 U.S.C. §119(e)

This application claims priority to the following provisional application(s):

| SERIAL NUMBER | FILING DATE |
|---------------|-------------|
| None | |

CERTIFICATE OF EXPRESS MAIL UNDER 37 C.F.R. §1.10

I hereby certify that this New Application Transmittal and the documents referred to as enclosed therein are being deposited with the United States Postal Service on this date November 24, 1998 in an envelope as "Express Mail Post Office to Addressee" Mailing Label Number

EL146971061US

addressed to the: Assistant Commissioner of Patents, Washington, D.C. 20231.

Linda M. White
Linda M. White

PTO
969861/60
11/24/98
JCS03 U.S. PTO

11/24/98
JC600 U.S. PTO

09198698 11/24/98

5. **Papers Enclosed Which Are Required For Filing Date Under 37 C.F.R. §1.53**

22 Pages of Specification, including claims and abstract
8 Sheets of Drawing

6. **Additional Papers Enclosed**

- ☒ Declaration and Power of Attorney
☐ Preliminary Amendment
☐ Information Disclosure Statement (37 CFR 1.98), Form PTO-1449 and a copy of each cited reference
☐ Assignment and Form PTO-1595
☒ Small Entity Declaration
This application is assigned to Massachusetts Institute of Technology
☐ Declaration of Biological Deposit
☐ Submission of "Sequence Listing" computer readable copy and/or amendment pertaining thereto for biotechnology invention containing nucleotide and/or amino acid sequences.
☐ Other _____

7. **Application Filing Fee Calculation**

A. ☒ Utility Application

FEE CALCULATION:

Total Claims: 9 - 20 = 0 × \$18 = \$ 0
Independent Claims: 3 - 3 = 0 × \$78 = \$ 0
Basic Fee: \$ 760
Multiple-Dependent-Claim Fee : \$

Total of the Above Calculations: \$ 760.00

0

- ☐ Amendment canceling extra claims enclosed.
☐ Amendment deleting multiple dependencies enclosed.
☐ Fee for extra claims is not being paid at this time.

B. ☐ Design application - \$310 \$
Application Filing Fee Sub-Total \$
C. ☒ Less 50% reduction for small entity..... \$-380.00
D. ☐ Non-English Specification - \$130..... \$

TOTAL FILING FEE \$380.00

8. **Payment**

- ☒ Enclosed
- ☒ Check in the amount of the Total Filing Fee set forth above.
- ☐ Charge Account No. 19-0079 in the amount of Total Filing Fee set forth above. A duplicate of this transmittal is attached.
- ☐ Not Enclosed

The Commissioner is hereby authorized to charge any fees under 37 C.F.R. §§1.16 and 1.17 that may be required by this paper or any paper filed in connection with this Patent Application, or refund any overpayment payable to Samuels, Gauthier & Stevens, LLP at the address set forth below.

Respectfully submitted,

Patrick O'Shea

Patrick J. O'Shea
Reg. No. 35,305
Samuels, Gauthier & Stevens LLP
225 Franklin Street, Suite 3300
Boston, MA. 02110

(617) 426-9180, Ext. 121

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Applicant or Patentee: Guy W. Carlisle
Serial or Patent No.: Attorney's Docket No.: MIT 8003L
Filed or Issued:
For: Imaging System with a Two-Axis-Gimbal Mirror Scan System Apparatus and Method

VERIFIED STATEMENT (DECLARATION) CLAIMING SMALL ENTITY STATUS
(37 CFR 1.9(f) and 1.27(d)) - NONPROFIT ORGANIZATION

I hereby declare that I am an official empowered to act on behalf of the nonprofit organization identified below:

NAME OF ORGANIZATION: Massachusetts Institute of Technology
ADDRESS OF ORGANIZATION: 77 Massachusetts Avenue
Cambridge, MA 02139
TYPE OF ORGANIZATION

- (X) UNIVERSITY OR OTHER INSTITUTION OF HIGHER EDUCATION
- () TAX EXEMPT UNDER INTERNAL REVENUE SERVICE CODE
(26 USC 501(a) and 501(c) (3))
- () NONPROFIT SCIENTIFIC OR EDUCATIONAL UNDER STATUTE OF
STATE OF THE UNITED STATES OF AMERICA
(NAME OF STATE _____)
(CITATION OF STATUTE _____)
- () WOULD QUALIFY AS TAX EXEMPT UNDER INTERNAL REVENUE
SERVICE CODE (26 USC 501(a) and 501(c) (3)) IF LOCATED IN THE
UNITED STATE OF AMERICA
- () WOULD QUALIFY AS NONPROFIT SCIENTIFIC OR EDUCATIONAL
UNDER STATUTE OF STATE OF THE UNITED STATES OF AMERICA
IF LOCATED IN THE UNITED STATES OF AMERICA
(NAME OF STATE _____)
(CITATION OF STATUTE _____)

I hereby declare that the nonprofit organization identified above qualifies as a nonprofit organization as defined in 37 CFR 1.9(e) for purposes of paying reduced fees under section 41(a) and (b) of Title 35, United States Code with regard to the invention entitled Imaging System with a Two-Axis-Gimbal Mirror Scan System Apparatus and Method by inventor(s) Guy W. Carlisle described in

- (X) the specification filed herewith.
- () application serial no. _____, filed _____.
- () patent no. _____, issued _____.

I hereby declare that rights under contract or law have been conveyed to and remain with the nonprofit organization with regard to the above identified invention.

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If the rights held by the nonprofit organization are not exclusive, each individual, concern or organization having rights to the invention is listed below* and no rights to the invention are held by any person, other than the inventor, who could not qualify as an independent inventor under 37 CFR 1.9 (c) if that person made the invention, or by any concern which would not qualify as a small business concern under 37 CFR 1.9(d) or a nonprofit organization under CFR 1.9(e). *NOTE: Separate verified statements are required from each named person, concern or organization having rights to the invention averring to their status as small entities. (37 CFR 1.27)

NAME _____
ADDRESS _____
() INDIVIDUAL () SMALL BUSINESS CONCERN () NONPROFIT ORGANIZATION

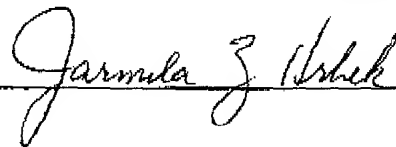
NAME _____
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I acknowledge the duty to file, in this application or patent, notification of any change in status resulting in loss of entitlement to small entity status prior to paying, or at the time of paying, the earliest of the issue fee or any maintenance fee due after the date on which status as a small entity is no longer appropriate. (37 CFR 1.28(b))

I hereby declare that all statements made herein of my own knowledge are true and that all statements made on information and belief are believed to be true; and further that these statements were made with the knowledge that willful false statements and the like so made are punishable by fine or imprisonment, or both, under section 1001 of Title 18 of the United States Code, and that such willful false statements may jeopardize the validity of the application, any patent issuing thereon, or any patent to which this verified statement is directed.

NAME OF PERSON SIGNING Jarmila Z. Hrbek
TITLE IN ORGANIZATION Patent Administrator and Office Manager,
Technology Licensing Office
ADDRESS OF PERSON SIGNING 77 Massachusetts Avenue, Room NE25-230
Cambridge, MA 02139

SIGNATURE



DATE

Nov 24, 1998

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UNITED STATES PATENT APPLICATION

of

GUY W. CARLISLE

for

**IMAGING SYSTEM WITH A TWO-AXIS-GIMBAL
MIRROR SCAN SYSTEM APPARATUS AND METHOD**

20160423160

IMAGING SYSTEM WITH A TWO-AXIS-GIMBAL MIRROR SCAN SYSTEM APPARATUS AND METHOD

5 GOVERNMENT RIGHTS

The government may have certain rights in this invention pursuant to United States Air Force Contract No. F19628-95-C-0002.

BACKGROUND OF THE INVENTION

10 The present invention relates to an orbital optical imaging system, and in particular to a method and apparatus that controls a scanning mirror, which provides a reflected image to a multiband (i.e., multiple spectral bands) focal plane array.

Satellites are widely used as platforms for various atmospheric monitoring instruments. For example, the United States National Oceanic and Atmospheric Administration (NOAA) operates a number of satellites that are used for weather monitoring. Some of these satellites operate in a geosynchronous orbit and regularly scan over predetermined areas of the Earth in order to monitor current weather conditions and provide data to weather forecasting systems.

The optical imaging instrument (an "imager") on these satellites includes several optical spectral bands that are used to monitor the weather. For example, there may be a visible imaging band and several infrared imaging bands. These various spectral bands together provide information regarding cloud cover and various forms of precipitation (e.g., rain, snow, sleet or hail) over the area of the Earth being monitored.

Technology improvements have recently made available large arrays comprising hundreds of optical detectors, that were not available when the current weather satellites were designed and manufactured. It is now possible to combine side-by-side, on a common surface, several long, line arrays of optical detectors, with each line array having detectors responsive to a particular spectral band. This assembly is often referred to as a multiband array of detectors. If this assembly of detectors is then installed on the focal plane of an optical instrument, the assembly is called a multiband focal plane array (MBFPA). For example, the MBFPA of a weather imager may include a visible band (e.g., 0.5 – 0.7 micrometers) and a number of infrared bands (e.g., eight bands over the range 1.8 – 13 micrometers).

An engineering obstacle to the use of a MBFPA in an advanced imager is the geometric distortion due to an optical effect known as “image rotation” that results if the MBFPA is used in combination with a conventional single-mirror scanning system. The purpose of the scanning system is to project a selected portion of the Earth (the “scene”) onto the MBFPA. In a conventional, single-mirror scanning system the mirror is first positioned relative to a first axis (e.g., to select the elevation of the scan), and then scanned about a second axis (e.g., azimuth) while holding the mirror position constant with respect to the first axis. The first and second axes are orthogonal. This scan process allows a user to select the Earth scene (usually in an automated sequence of scans) to be viewed by the imaging instrument. The scanning process can be repeated in a progressive sequence to obtain a multi-spectral image of the full Earth disk.

However, the use of a conventional, single-mirror scan system in combination with the MBFPA causes two undesirable errors. The first error is a pixel-to-pixel *registration* error within a frame, which is a geometrical distortion in which the pixels within an image frame are misaligned with respect to each other, such that they are not "observed" at their true positions in the Earth scene. The second error is a band-to-band *coregistration* error. The coregistration error is a geometrical effect in which the detectors in different spectral line arrays of the MBFPA do not traverse the same area of the Earth scene during the scan. Both of these errors have an adverse effect on the quality of weather imagery. Therefore, a technique is needed to image an Earth scene onto the MBFPA without introducing the registration and coregistration errors in order to utilize the new MBFPA technology effectively. Several techniques are currently under investigation.

One technique is to use an assemblage of multiple beamsplitters to split the incoming light flux onto a series of separate, single-band focal plane arrays of detectors. However, this technique does not enable the use of the MBFPA since the separate focal planes have detectors of only a single spectral imaging band. In addition, this technique does not correct for the pixel-to-pixel registration error. This design approach is also relatively costly and complex due to the precision required in the physical alignment and calibration of the assemblage of beamsplitters.

A second approach under consideration is to use two cascaded scanning mirrors. The first mirror would scan about a first axis (e.g., scan in elevation), while the second mirror would scan about a second axis (e.g., scan in azimuth). This approach would correct both

registration and coregistration errors and, indeed, enable the use of the MBFPA technology.

However, since the mirror is a heavy component of the imager, adding an additional mirror is undesirable because it adds to the mass and bulk of the satellite. Significantly, it adds to the launch mass of the satellite.

5 Therefore, there is a need for an imaging system comprising a MBFPA that is free from the undesirable geometrical errors of image registration and coregistration.

SUMMARY OF THE INVENTION

10 Briefly, according to the present invention, a mirror is scanned to provide an image of a desired portion of the Earth to a multiband focal plane array (MBFPA). The mirror is first positioned relative to a first axis (e.g., elevation) as a starting position of the image scan. The mirror is then scanned about a second axis and repositioned relative to the first axis while scanning the mirror about the second axis (e.g. azimuth).

15 This invention may be used in a satellite-based weather imaging instrument to remove registration and coregistration errors that occur when a conventional, single-mirror scan system is used in combination with the MBFPA. The present invention positions the mirror relative to the first axis (e.g., the elevation at the start of the scan), and while scanning the mirror about the second axis (e.g., azimuth), the mirror is repositioned in a controlled manner relative to the first axis. That is, the invention dynamically adjusts the position of the mirror relative to the
20 first axis while scanning about the second axis. Scanning about the first axis may be an elevation scan while scanning about the second axis may be an azimuth scan, or vis-a-versa.

Advantageously, this control technique ensures that the images within each spectral band are spatially registered pixel-by-pixel within the image frame, and that the images of the various spectral bands are spatially coregistered with respect to each other. The present invention provides a scan-control technique for a single-mirror scan system that enables the use of the MBFPA in an imaging instrument.

These and other objects, features and advantages of the present invention will become apparent in light of the following detailed description of preferred embodiments thereof, as illustrated in the accompanying drawings.

BRIEF DESCRIPTION OF THE DRAWINGS

FIG. 1 is a pictorial illustration of a satellite-based imaging system positioned over the Earth;

FIG. 2 is a pictorial illustration presenting the image rotation in terms of the "equivalent" rotation of a line vector;

FIG. 3 illustrates a contour plot of θ as a function of azimuth angle A and elevation angle E ;

FIG. 4 illustrates the effect of "image rotation" on pixel-to-pixel registration error within a frame;

FIG. 5 illustrates the geometry of the MBFPA showing an effective "rotation" due to the scanning of the mirror (FIG. 1) that provides an image to the MBFPA;

FIG. 6 is an illustration of how scanning the mirror (FIG. 1) in azimuth across the

Earth disk while holding the elevation of the mirror constant, causes the detectors of the various bands of the MBFPA to pass through a given geodetic longitude L_G ;

FIG. 7 is a plot of the mirror elevation position versus azimuth position illustrating the taper in elevation as a function of azimuth; and

FIG. 8 illustrates a flow chart illustration of a mirror control routine.

DETAILED DESCRIPTION OF THE INVENTION

FIG. 1 is a pictorial illustration of a satellite-based imaging system 10 positioned over the Earth 12. The imaging system 10 includes a mirror 14 having a reflective surface 15 that provides a reflected image of an area of the Earth onto a multiband focal plane array (MBFPA) 16. The MBFPA 16 includes a plurality of distinct optical imaging spectral bands 18-21 that each includes a plurality of detectors. The first band 18 may be a visible imaging band while the other bands 19-21 are infrared bands each operating at a slightly different wavelength (e.g., in the range of about 1.8 - 13 micrometers). The imaging system 10 may be used in a weather satellite.

The mirror 14 rotates in a limited range about a first axis 22 and limited range about a second axis 23, in order to provide a reflected image of a selected area of the Earth. Rotation about the first axis 22 scans the mirror 14 in elevation, while rotation of the mirror about the second axis 23 provides the ability to scan the mirror 14 in azimuth. The system 10 also includes a scan controller 24 that provides signals on lines 25, 26 to actuators 27, 28 that position the mirror about the first and second axes 22, 23, respectively. The system 10 may

use an open or closed loop control system architecture to position and scan the mirror 14. We shall now briefly describe the optical effect known as "image rotation" that is a source of registration and coregistration errors.

FIG. 2 is a pictorial illustration 30 presenting the image rotation analytically modeled in terms of the "equivalent" rotation of a line vector, \bar{L} 32, in the MBFPA as projected onto a flat Earth. Alternatively, one of ordinary skill will recognize that it is also possible to model the image rotation as the projection of the Earth scene on the focal plane and to extend the analysis to the geometry of a spherical Earth. For the modeling we use the *method of images* to replace the line vector \bar{L} 32 with its image vector, \bar{I} 34 (this technique is often used to solve electrostatics problems which are analytically analogous). This technique allows us to use the image vector \bar{I} 34 to calculate the line vector's projection onto the Earth, as though the image vector \bar{I} 34 were in free space, thus removing the complication of the mirror's presence. In the calculation, an important parameter is the mirror's normal, \hat{n} 36. We can express the image vector \bar{I} 34 in terms of the normal \hat{n} 36 and use the normal \hat{n} to keep track of the mirror's 14 orientation during the scanning process. In the scan process, the normal \hat{n} 36 becomes a function of the North-South elevation, E , and the East-West azimuth, A . We shall now discuss an elevation rotation of the mirror 14 (i.e., a N-S scan).

First consider the image rotation in the case of an elevation scan (i.e., a N-S scan) in which azimuth $A = 0$ while elevation E varies. Referring to FIG. 2, we can express the image

as $\bar{I} = I_n \hat{n} + I_p \hat{p}$ where $I_n = -\hat{n} \cdot \bar{L}$ and $I_p = \hat{p} \cdot \bar{L}$. At $E = 0$ (nadir), the normal is $\hat{n}_0 = \frac{-\hat{y} + \hat{z}}{\sqrt{2}}$.

For a N-S scan, through an angle E about the \hat{z} -axis, $\hat{n} = \frac{-\sin E \hat{x} - \cos E \hat{y} + \hat{z}}{\sqrt{2}}$. The

companion unit vector, \hat{p} 38, is given by $\hat{p} = \frac{(\hat{n} \times \bar{L}) \times \hat{n}}{|(\hat{n} \times \bar{L}) \times \hat{n}|}$. From the above relationships, after

some manipulation, the image vector \bar{I} can be expressed as:

$$\bar{I} = L(-\sin E \cos E \hat{x} + \sin^2 E \hat{y} + \cos E \hat{z}). \quad (\text{EQ. 1})$$

The rotation angle of the line vector \bar{L} is given by:

$$\theta = \tan^{-1} \left(\frac{\hat{x} \cdot \bar{I}}{\hat{z} \cdot \bar{I}} \right) \quad (\text{EQ. 2})$$

Using the expression for \bar{I} in EQ. 1, EQ. 2 can be rewritten as:

$$\theta = -\tan^{-1}[\sin E] \quad (\text{EQ. 3})$$

At this point in the analysis the scan is limited to a scan in E only. At the small values E , $\theta \approx -E$, which is the case at geostationary orbit where approximately $E \leq 8^\circ$.

The extension of the analysis to scan in both elevation E and azimuth A proceeds in a similar manner. After some mathematics, we obtain the following expression for the rotation angle θ :

$$\theta = \tan^{-1} \left[\sin E \tan \left(A - \frac{\pi}{4} \right) \right] \quad (\text{EQ. 4})$$

FIG. 3 illustrates a contour plot 40 of θ as a function of A and E , as calculated from EQ. 4.

The azimuth angle A is plotted along a horizontal axis 41 and elevation angle E is plotted along a vertical axis 42. Note that, to very close approximations, the scan mirror's azimuth encoder angle, A , is one-half of the pointing angle in the azimuth direction while the elevation encoder angle E is equal to the pointing angle in the elevation direction, such that, a range of rotation of approximately $(-4^\circ \leq A \leq 4^\circ)$ and $(-8^\circ \leq E \leq 8^\circ)$ provides full coverage of the Earth disk, as viewed from geostationary orbit. We now have the mathematical tools in place to calculate the registration and coregistration errors caused by image rotation.

First, we calculate the registration error. FIG. 4 illustrates the effect of image rotation on pixel-to-pixel registration within an image frame. In the interest of simplicity, only three points (A,B,C) 43-45 on the Earth and three detectors 46-48 in a line array 49 (of a particular spectral band) that "correspond" to observation of these points are illustrated. The points (A,B,C) 43-45 are the "true" locations of these points in the scene, and the corresponding detectors 46-48 are the "observed" locations of the points. If the three points (A,B,C) 43-45 lay in the centers of their corresponding detectors 46-48, the pixels are registered; if not, there is a registration error.

Referring still to FIG. 4, in scan #1 49 at the Equator ($E_1 = 0$), there is zero image rotation, and the points (A,B,C) 43-45 are aligned with their corresponding detectors 46-48.

That is, there is no registration error because the "true" and "observed" locations of the points coalesce.

In contrast, in scan #2 50 at a location above the Equator ($E_2 > 0$), the image rotation displaces the location of the points (A, C) 43, 45 from their corresponding detectors 46, 48, respectively. This effect causes a registration error, as shown in the "blow-up" of FIG. 4. The amount of registration error increases with elevation (i.e., at more northerly scans), where the image rotation increases in magnitude.

The registration error is given mathematically by:

$$\text{Error} = L/2 \sin \theta \quad (\text{EQ. 5})$$

In EQ. 5, the quantity L is the scan swath width, which is the projection of a N-S line array onto the Earth, and θ is the image rotation angle.

As a numerical example, assume an array length of $1/2^\circ$, for which $L = 568$ km. At an elevation of $E = 4^\circ$ (i.e., an Earth scene centered at a geodetic latitude of approximately 23.6°) along the geodetic longitude that passes through the satellite's nadir point, we calculate from EQ. 5 a registration error of approximately 20 km. Extending this result (for a single swath) to a 2000-km by 2000-km image gives a registration error of approximately 40 km at $E = 4^\circ$, which exceeds typical requirements in weather imaging.

Next, we consider the band-to-band coregistration error. FIG. 5 illustrates the geometry of the "rotation" of the MBFPA 16 due to the orientation of the scanning mirror 14

(FIG. 1), that provides an image of the Earth scene to the MBFPA. One of ordinary skill will recognize that the effective "rotation" of the MBFPA is a modeling construct of the analysis. The MBFPA does not actually rotate; rather, it is the scan mirror's reflection of the Earth scene onto the MBFPA that rotates while the MBFPA remains stationary. The line arrays of the optical imaging bands of the MBFPA 16 nominally extend in the N-S direction in the absence of image rotation, as in the azimuth scan centered on the Equator. Scanning the mirror in elevation at geodetic latitudes above the Equator causes the projection of the Earth scene on the MBFPA to rotate through angle θ , which can be modeled as an "effective" rotation of the MBFPA, as depicted in FIG. 5.

In FIG. 5 we see that the effective rotation of the MBPFA 16 causes a *coregistration* error to occur between corresponding detectors 52-54 of the various spectral bands 18-21, respectively. "Corresponding" detectors refers to detectors of different spectral bands that would trace the same geodetic latitude in the absence of image rotation. For example, a set of "corresponding" detectors are the detectors 52-54. The coregistration error between the corresponding detectors of two different spectral bands, spatially separated in the MBFPA by the distance, D , is given by the following expression:

$$Error = \frac{D}{\Delta} \sin \theta \times 100\% \quad (EQ. 6)$$

where Δ is the dimension of the square detector. In EQ. 6, the coregistration error is normalized by Δ . Referring still to FIG. 5, the largest coregistration error occurs between the spectral bands that are the farthest apart in the MBFPA (i.e., bands 18 and 21). In this case, $D = W - \Delta$, where W is equal to the width of the MBFPA. As an example, if $\Delta = 45 \mu\text{m}$ and $W = 14.7 \text{ mm}$, then the coregistration error between bands 18 and 21 is approximately 2300% at an elevation of $E = 4^\circ$ (a point at a geodetic latitude of approximately 23.6°). This coregistration error grossly exceeds the error limits of a weather imaging system of acceptable image quality and indicates the need for the present invention. We shall now describe how the present invention eliminates the band-to-band coregistration error.

Referring to FIG. 6, scanning the mirror 14 (FIG. 1) in azimuth 60 across the Earth disk while holding the elevation of the mirror constant, causes the detectors of the various bands 18-21 of the MBFPA to pass through a given geodetic longitude L_G 62 at a different geodetic latitude. For example, during the azimuth scan the detector 52 $D-I$ passes through L_G 62 at a slightly higher geodetic latitude than when the detector 56 $D-N$ passed through L_G 62 and, in fact, this effect is the source of the band-to-band coregistration error. The consequence of the error is that the corresponding detectors of various spectral bands do not traverse the same point ("spot") in an Earth scene during the scan. According to the present invention, during each scan the elevation of the scanning mirror 14 (FIG. 1) is also controlled as a function of the scan position in elevation and azimuth, such that when the detector 52 $D-I$ reaches L_G 62, it is at the same geodetic latitude at which the detector 56 $D-N$ passed through L_G . Tapering the elevation of the scan versus position of the scan mirror in this way removes

the coregistration error by ensuring that the detectors of each spectral band in the MBFPA sample their data at identical geodetic sample points in the Earth scene. Accordingly, the scan process of this invention removes the effect of image rotation and brings the various spectral bands of the MBFPA into coregistration. We shall now quantitatively discuss the present invention.

Since $dE/dA = \tan \theta$, the required elevation taper as a function of scan position (the azimuth A and elevation E_w) is given by:

$$E = E_w + \int_{A_w}^A \tan \theta dA \quad (\text{EQ. 7})$$

where E_w and A_w are the discrete elevation and azimuth settings, respectively, at the beginning of the scan. From EQ. 4 we see that the integrand in EQ. 7 can be expressed as:

$$\tan \theta = \sin E \tan(A - \frac{\pi}{4}). \quad (\text{EQ. 8})$$

Substitution of (EQ. 8) into (EQ. 7) yields:

$$E = E_w + \sin E \int_{A_w}^A \tan(A - \frac{\pi}{4}) dA . \quad (\text{EQ. 9})$$

Evaluating the integral in EQ. 9 we obtain:

$$E = E_w - \sin E \ln \left[\frac{\cos(A - \frac{\pi}{4})}{\cos(A_w - \frac{\pi}{4})} \right] \quad (\text{EQ. 10})$$

We see that the right most term of EQ. 10 is the mirror elevation taper versus azimuth that is required to prevent/reduce coregistration errors. We can solve EQ. 10 for E by either numerical iteration or a technique using a Taylor series expansion of $\sin E$. The latter technique works best if we first rearrange EQ. 10 to exploit the rapid convergence of a Taylor series if cast in terms of a variable whose magnitude is small. Accordingly, we introduce the variable $x = E - E_w$ and rewrite EQ. 10 as:

$$x = \sin(x + E_w) f_A \quad (\text{EQ. 11})$$

where for convenience we define $f_A = -\ln \left[\frac{\cos(A - \frac{\pi}{4})}{\cos(A_w - \frac{\pi}{4})} \right]$. We can use a trigonometric

identity to rewrite EQ. 11 as:

$$x = (\cos E_w \sin x + \sin E_w \cos x) f_A \quad (\text{EQ. 12})$$

Expanding the terms of EQ. 12 involving x as a Taylor series yields:

$$x = [\cos E_w (x - x^3/3! + \dots) + \sin E_w (1 - x^2/2! + \dots)] f_A \quad (\text{EQ. 13})$$

The convergence is rapid because $|x| \ll 1$. Accordingly, we omit terms in x higher than

5 second order to obtain the quadratic equation:

$$x^2 + bx + c = 0 \quad (\text{EQ. 14})$$

where

$$b = 2 \frac{1 - f_A \cos E_w}{f_A \sin E_w} \quad (\text{EQ. 15a})$$

$$c = -2 \quad (\text{EQ. 15b})$$

From the definition of x we obtain:

$$E = E_w + x_p \quad (\text{EQ. 16})$$

where x_p , the elevation taper, is given by the appropriate root of EQ. 14. It should be noted that we have also solved EQ. 13 by keeping the third-order terms in x and found negligible change in the results. Alternative solutions based on numerical iteration can be used to solve

20 EQ. 10 for E to arbitrary accuracy.

FIG. 7 is a plot 70 of mirror elevation position versus azimuth encoder position based upon EQ. 16, illustrating the taper in elevation as a function of azimuth (the "jaggies" evident in the curves are not real but rather an artifact of the software/printer used to generate the plot). Azimuth encoder angle A is plotted along a horizontal axis 72 and elevation angle E is plotted along a vertical axis 74. We shall now briefly describe the operational control of the mirror 14 (FIG. 1).

FIG. 8 is a flow chart illustration of a mirror control routine 80. The routine 80 can be performed as a series of programmable software steps executed by the control logic of the scan controller 24 (FIG. 1). Referring to FIGs. 1, 7 and 8, a first step 82 in the routine 80 is to position the mirror 14 (e.g., in a discrete step which depends on the swath width of the line arrays in the MBFPA) with respect to the first axis 22 (FIG. 1). This position is based upon the location in elevation of the desired Earth scene to be imaged in the scanning process. The scan controller 24 determines the elevation angle at which the mirror 14 must be placed relative to the first axis 22 to image the desired Earth scene, and provides a command signal on the line 25 to position the mirror accordingly. As an example, this initial elevation position is shown in FIG. 7 as starting point 84. Once the mirror 14 is in the desired elevation position relative to the first axis 22, step 86 is then executed to scan the mirror about the second axis 23 in azimuth. According to the present invention, step 88 is then executed to adjust the position of the mirror in a prescribed way relative to the first axis 22 as the mirror continues to scan about the second axis 23. That is, referring to FIG. 7, as the mirror begins to scan in azimuth from the starting point 84, the scan controller 24 (FIG. 1) commands the mirror to follow line

90. Significantly, as the mirror scans in azimuth, the scan controller also commands the elevation actuator 28 so the mirror position tracks the prescribed elevation "taper" along line 90. At the end of the azimuth scan, the mirror will be at end position 92. The scan controller then commands the mirror to position 94 and begins scanning from right-to-left along line 96.

5 Controlling the mirror position with respect to the first axis 22 as the mirror rotatably scans about the second axis 23 ideally eliminates both the registration and coregistration errors. This is an example of the scan process. The actual size of the scan steps in elevation (one degree in this example) will depend on the length of the line arrays of the MBFPA used in the instrument.

10 The elevation taper of the present invention causes the swaths of successive scans to overlap in coverage slightly, which varies gradually in amount over the course of the azimuth scan. Simple data editing to remove or average out redundant pixels in the overlapped regions corrects this effect. Editing options include disregarding the "old" pixels of the previous scan in favor of the "new" pixels of the present scan (or vice versa), or averaging or weighting the

15 "new" and "old" overlapped pixels. Although the present invention has been primarily discussed in the context of initially setting the position of the mirror with respect to elevation, and then scanning in azimuth while elevation is changed as a function of scan position, one of ordinary skill in the art will recognize that the roles of the two axes can be reversed. For example, the scan may occur in elevation and the azimuth position is controlled as a function

20 of scan mirror's position.

Although the present invention has been shown and described with respect to several preferred embodiments thereof, various changes, omissions and additions to the form and detail thereof, may be made therein, without departing from the spirit and scope of the invention.

5 What is claimed is:

CLAIMS

1 1. A method of scanning a mirror that provides an image of a portion of the Earth to a
2 multiband focal plane array of optical detectors in an imager, the method comprising the steps:
3 positioning the mirror relative to a first axis;
4 scanning the mirror about a second axis; and
5 repositioning the mirror relative to the first axis while scanning the mirror about the
6 second axis.

1 2. The method of claim 1, further comprising the step of:
2 selecting a desired location on the Earth to be imaged by the multiband focal
3 plane array of optical detectors and providing a first axis control signal indicative of the
4 position for the mirror relative to the first axis in order to image the desired location on the
5 Earth.

1 3. The method of claim 1, wherein the first and second axes are perpendicular to a
2 reflective plane of the mirror that provides the image to the multiband focal plane array of
3 optical detectors in an imager.

1 4. The method of claim 2, wherein when the mirror is positioned about the first axis to set
2 the scan elevation and the mirror scans in azimuth as it moves about the second axis.

1 5. The method of claim 2, wherein when the mirror is positioned about the first axis to set
2 the scan azimuth and the mirror scans in elevation as it moves about the second axis.

1 6. A method of controlling the position of a planar mirror in an orbital weather imaging
2 system to provide a reflected image to a multiband focal plane array of optical detectors in an
3 imager, the method comprising the steps of:

4 positioning the mirror relative to a first axis;

5 positioning the mirror relative to a second axis; and

6 scanning the mirror relative to the first axis while repositioning the mirror relative to
7 the second axis as a function of the mirror position relative to the first axis, to reduce
8 registration and coregistration errors provided by the multiband focal plane array of optical
9 detectors.

1 7. An orbital weather imaging system that images a selected portion of the Earth onto a
2 multi-spectral-band array of optical detectors on a focal plane that is displaced in angle from
3 the plane of the scene, while compensating for the rotation of the scene's image on the focal
4 plane with respect to the actual scene to maintain the registration of pixel location in each
5 image frame, and maintain the coregistration among the spectral bands in the focal plane array
6 during the scan of the selected portion of the Earth, the system comprising:

7 a focal plane array having a plurality of imaging bands;

8 a mirror mounted to scan in elevation and in azimuth and provide a reflective image of

9 the Earth scene onto said focal plane array; and

10 a controller that commands said mirror to a starting elevation position and to a starting
11 azimuth position, and then scans said mirror in elevation while also scanning said mirror in
12 azimuth.

1 8. The orbital weather imaging system of claim 7, wherein said controller comprises:

2 a mirror azimuth position sensor that provides an azimuth position signal;

3 a mirror elevation position sensor that provides an elevation position signal;

4 an electronic controller responsive to said azimuth position signal, said elevation
5 position signal and a signal indicative of the area to be imaged, to compute an azimuth
6 command signal and an elevation command signal;

7 a first actuator responsive to said azimuth command signal to position said mirror in
8 azimuth; and

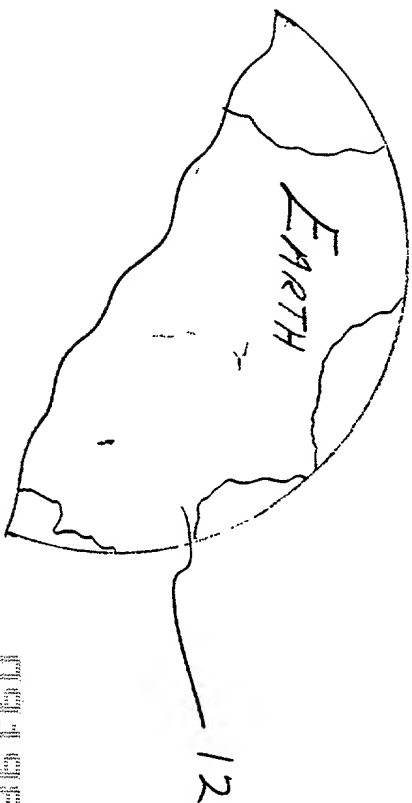
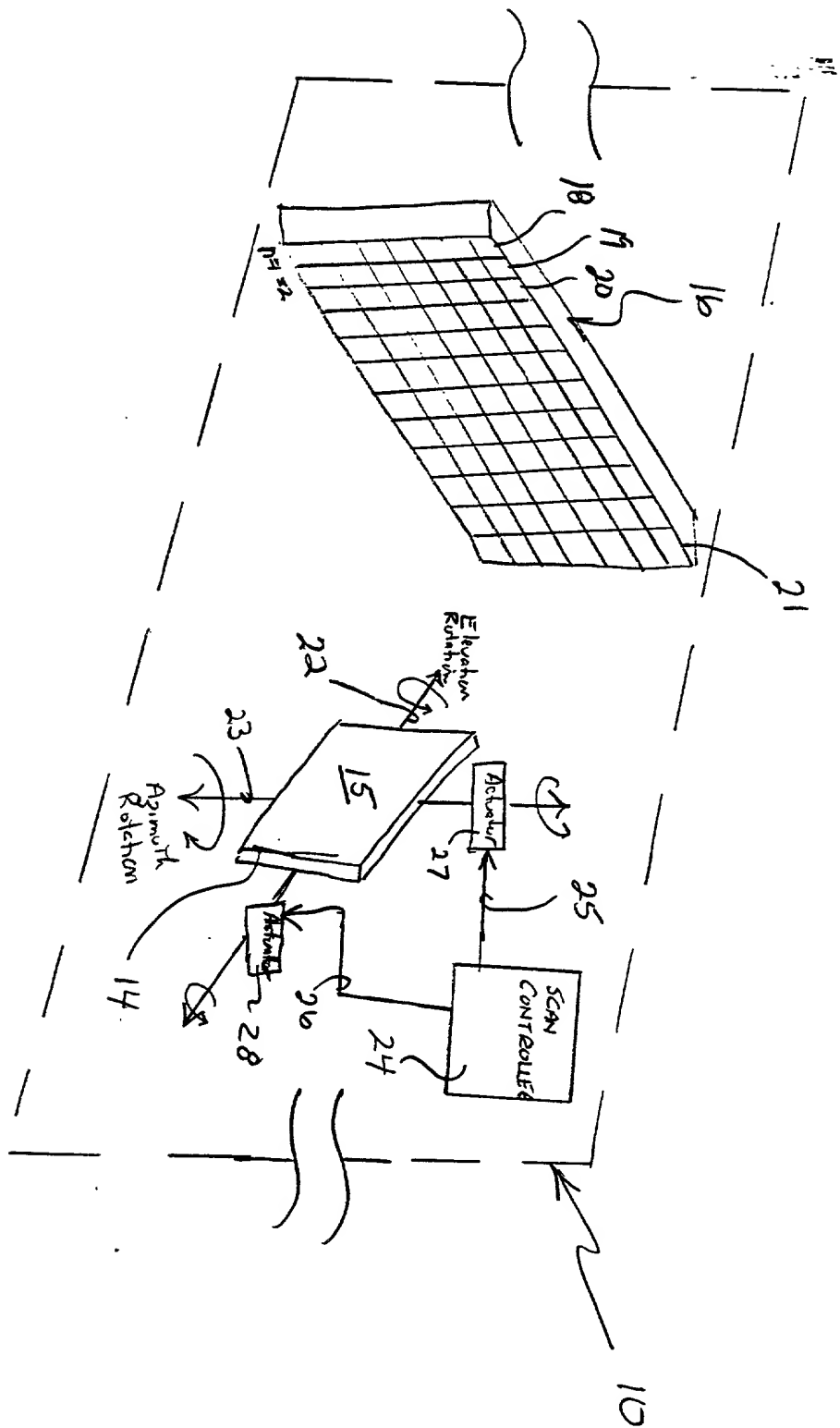
9 a second actuator responsive to said elevation command signal to position said mirror in
10 elevation.

1 9. The orbital weather imaging system of claim 8, wherein said focal plane array includes

2 a visible imaging band and a plurality of infrared imaging bands.

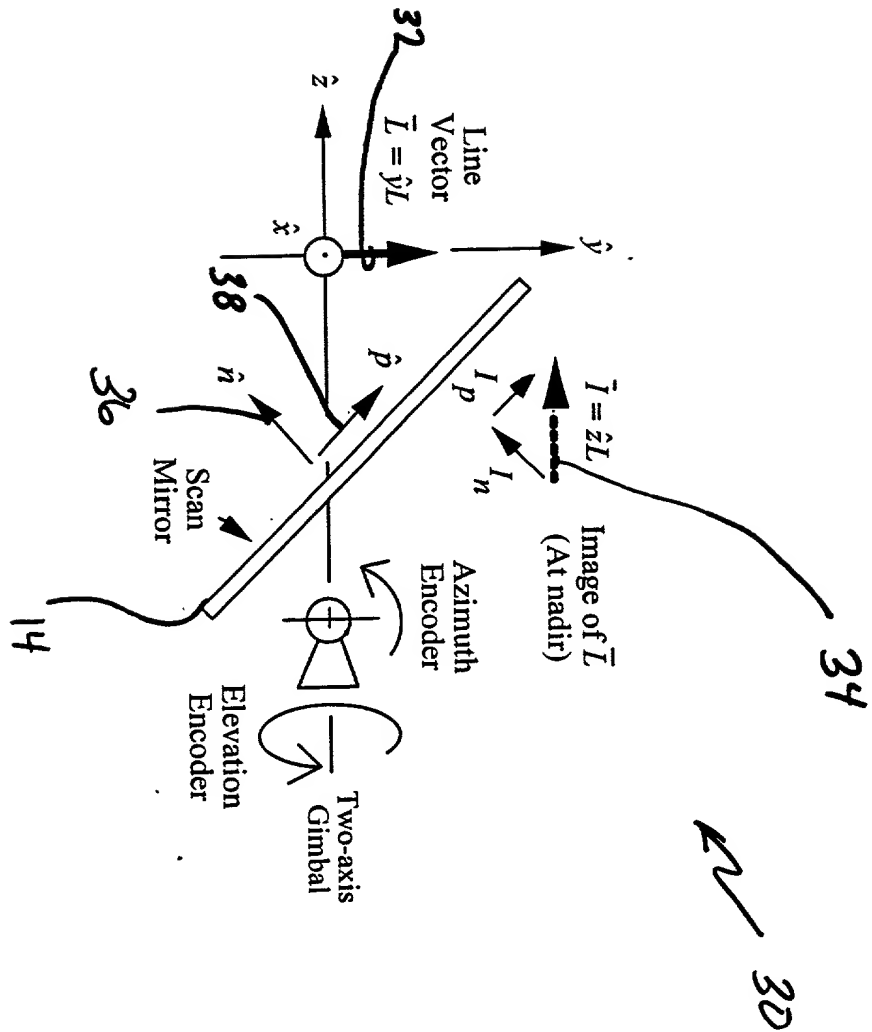
ABSTRACT

A mirror is scanned to provide an image of a portion of the Earth to a multiband focal plane array (MBFPA) of optical detectors (an "imager"). Initially, the mirror is positioned relative to a first axis. The mirror is then scanned about a second axis and repositioned relative to the first axis while scanning the mirror about the second axis. This invention may be used in a weather satellite to remove prevent/reduce errors in pixel-to-pixel registration within an image frame and errors in band-to-band that occur when the various imaging bands (e.g., visual and infrared) of the MBFPA are used to image or scan selected areas of the Earth. The present invention positions the mirror relative to the first axis (e.g., elevation), and while scanning the mirror about the second axis (e.g., azimuth), the mirror is regularly repositioned in a prescribed manner relative to the first axis. That is, the invention dynamically adjusts the position of the mirror relative to the first axis while scanning about the second axis. Scanning about the first axis may be an elevation scan while scanning about the second axis may be an azimuth scan, or vis-a-versa. Advantageously, this control technique ensures that the images within each spectral band are spatially registered pixel-by-pixel within the image frame, and that the images of the various spectral bands are spatially coregistered with respect to each other. The present invention provides a scan-control technique for a single-mirror scan system that enables the use of the MBFPA in an imaging instrument.



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FIG. 1

FIG. 2

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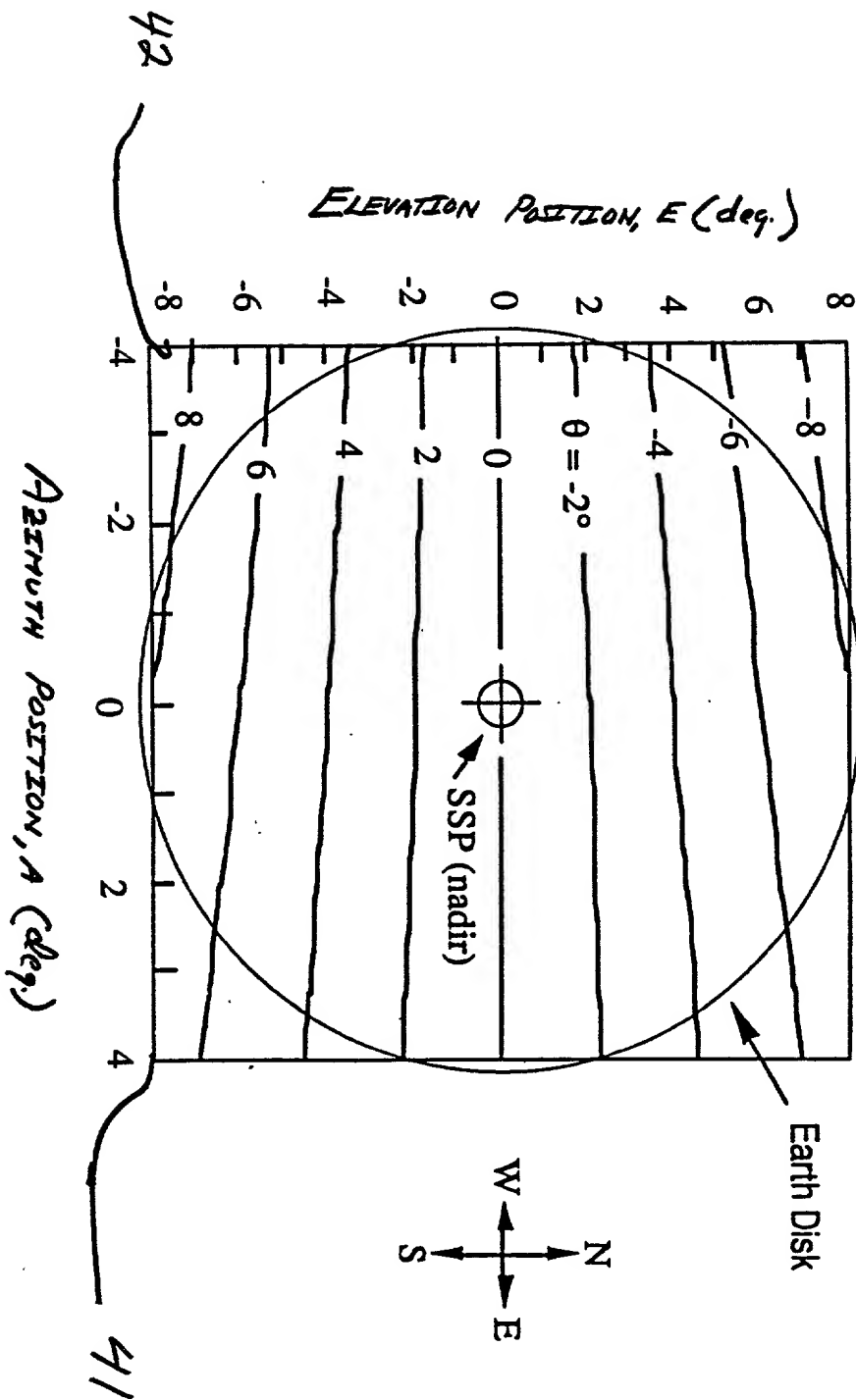


FIG. 3

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FIG. 4

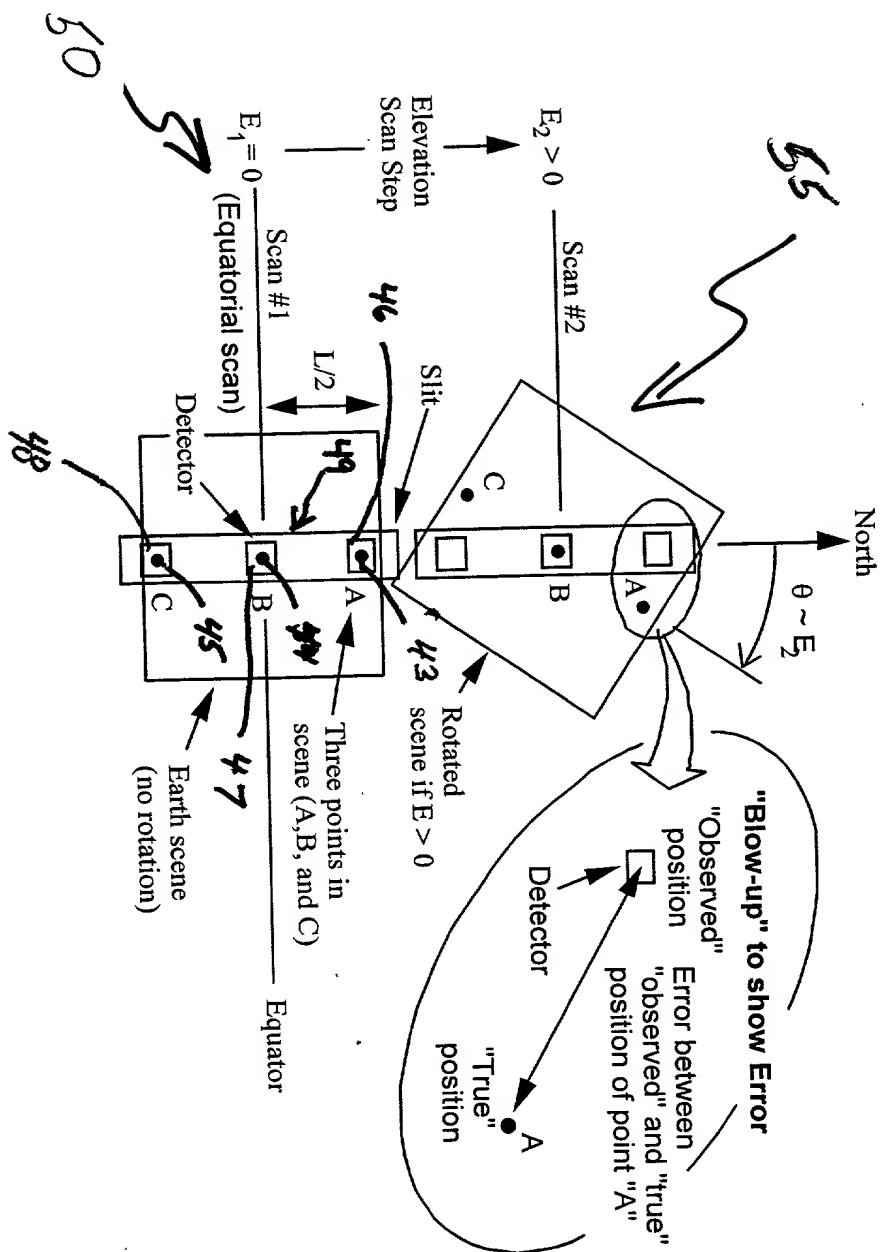
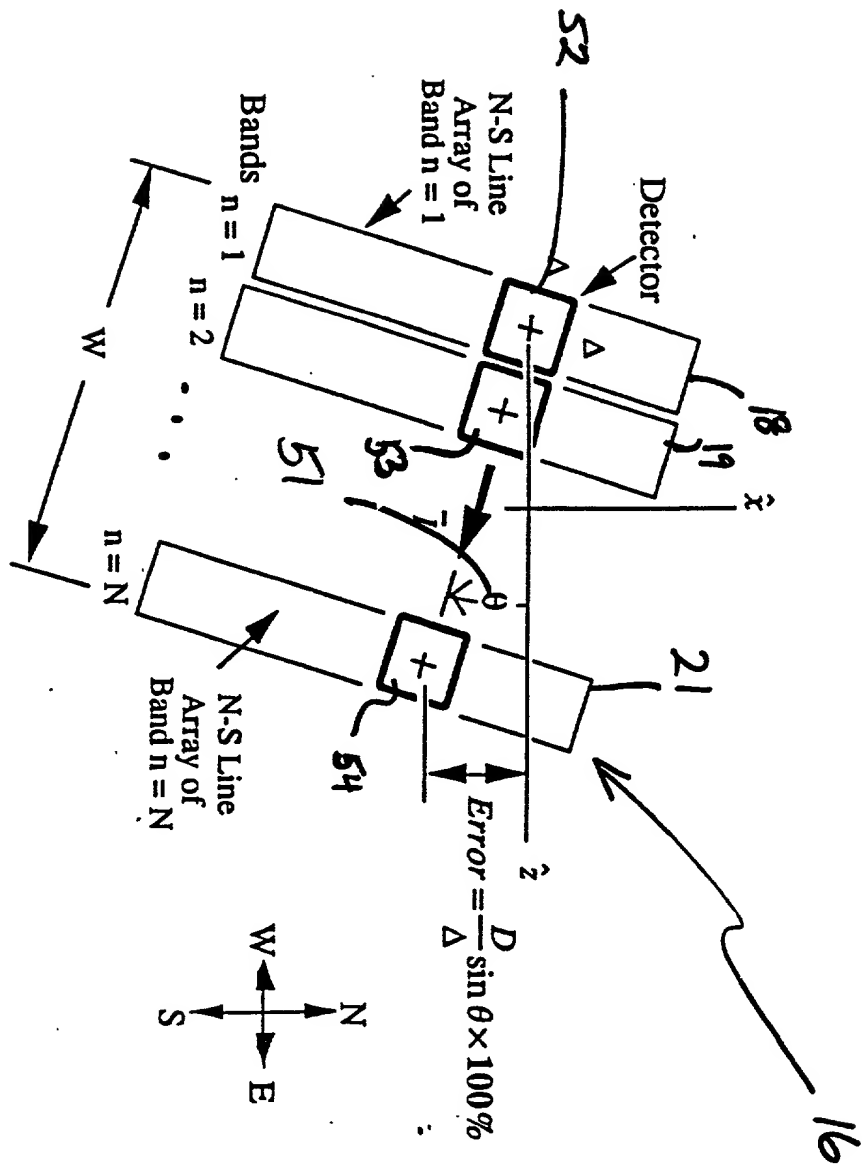
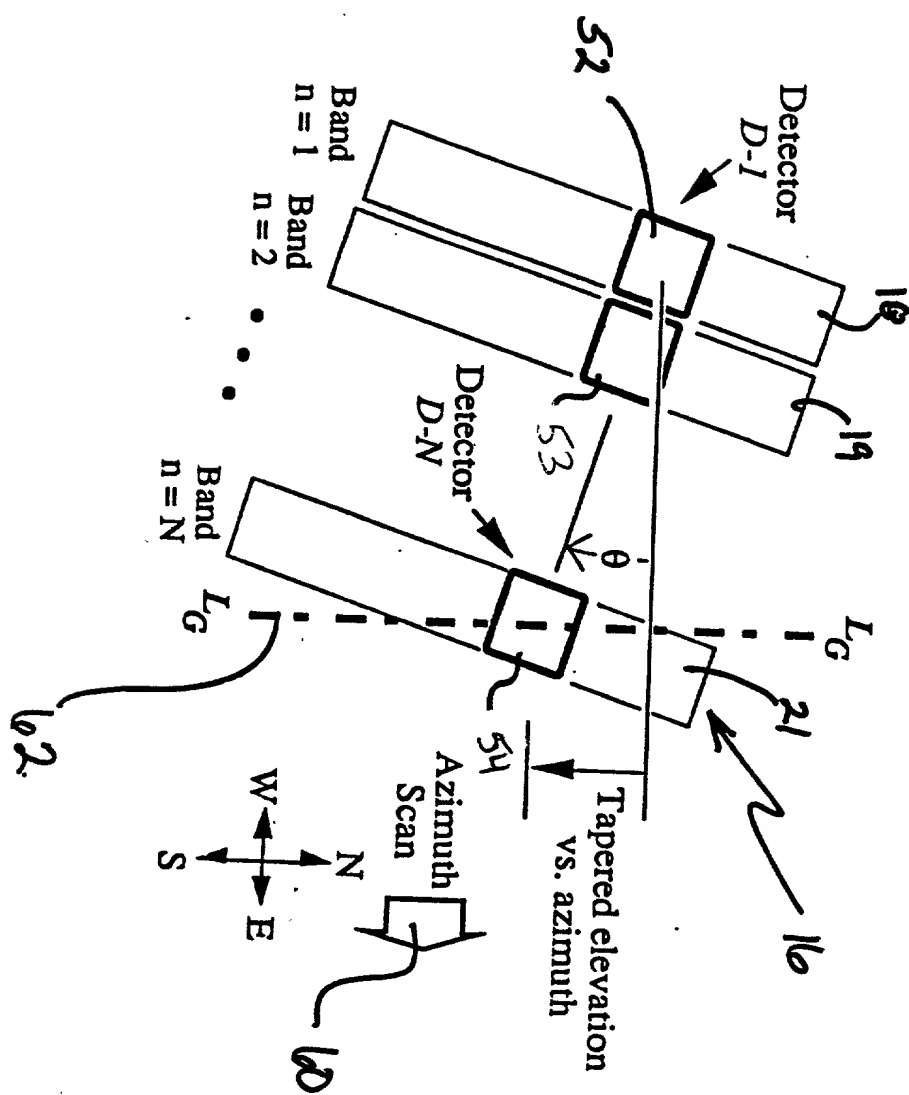


FIG. 5





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| Climatic data | | Soil data | | Vegetation data | | Water data | | Air data | |
|----------------------|----------|---------------------|---------|---------------------------|------------|------------------------------|-------|-----------------|----------|
| Variable | Unit | Variable | Unit | Variable | Unit | Variable | Unit | Variable | Unit |
| Temperature | °C | Soil moisture | % | Vegetation cover | % | Water level | m | Air quality | ppm |
| Humidity | % | Soil pH | pH | Vegetation height | m | Water flow | m³/s | Air pressure | hPa |
| Wind speed | m/s | Soil temperature | °C | Vegetation density | plants/m² | Water temperature | °C | Air temperature | °C |
| Wind direction | ° | Soil salinity | g/kg | Vegetation biomass | kg/m² | Water quality | ppm | Air humidity | % |
| Cloud cover | % | Soil texture | cm | Vegetation species | species/m² | Water pH | pH | Air pollution | ppm |
| Cloud height | m | Soil depth | cm | Vegetation age | years | Water salinity | g/kg | Air noise | dB |
| Cloud color | RGB | Soil porosity | % | Vegetation health | index | Water turbidity | NTU | Air vibration | m/s² |
| Cloud shape | area | Soil permeability | cm/s | Vegetation growth | cm/year | Water conductivity | µS/cm | Air radiation | µSv/h |
| Cloud size | km² | Soil compaction | kg/cm² | Vegetation loss | %/year | Water viscosity | cP | Air magnetism | gauss |
| Cloud mass | kg | Soil erosion | cm/year | Vegetation recovery | %/year | Water surface tension | N/m | Air gravity | g |
| Cloud volume | m³ | Soil degradation | %/year | Vegetation regeneration | %/year | Water capillary action | cm | Air buoyancy | N |
| Cloud density | kg/m³ | Soil restoration | %/year | Vegetation succession | %/year | Water osmotic pressure | MPa | Air adhesion | N |
| Cloud composition | chemical | Soil conservation | %/year | Vegetation adaptation | %/year | Water surface area | m² | Air cohesion | N |
| Cloud behavior | pattern | Soil management | %/year | Vegetation resilience | %/year | Water surface volume | m³ | Air friction | N |
| Cloud interaction | network | Soil monitoring | %/year | Vegetation sustainability | %/year | Water surface weight | N | Air resistance | N |
| Cloud communication | protocol | Soil analysis | %/year | Vegetation productivity | %/year | Water surface mass | kg | Air inertia | kg·m²/s² |
| Cloud energy | J | Soil synthesis | %/year | Vegetation efficiency | %/year | Water surface energy | J | Air momentum | kg·m/s |
| Cloud power | W | Soil transformation | %/year | Vegetation effectiveness | %/year | Water surface force | N | Air impulse | N·s |
| Cloud energy density | J/m³ | Soil regeneration | %/year | Vegetation impact | %/year | Water surface pressure | Pa | Air torque | N·m |
| Cloud power density | W/m³ | Soil rejuvenation | %/year | Vegetation influence | %/year | Water surface stress | Pa | Air work | J |
| Cloud energy flux | W/m² | Soil revitalization | %/year | Vegetation effect | %/year | Water surface tension force | N | Air heat | J |
| Cloud power flux | W/m² | Soil rejuvenation | %/year | Vegetation outcome | %/year | Water surface energy density | J/m³ | Air work rate | W |
| Cloud energy rate | W | Soil restoration | %/year | Vegetation result | %/year | Water surface energy rate | W | Air work rate | W |
| Cloud power rate | W | Soil conservation | %/year | Vegetation achievement | %/year | Water surface energy rate | W | Air work rate | W |
| Cloud energy rate | W | Soil management | %/year | Vegetation success | %/year | Water surface energy rate | W | Air work rate | W |
| Cloud power rate | W | Soil monitoring | %/year | Vegetation fulfillment | %/year | Water surface energy rate | W | Air work rate | W |
| Cloud energy rate | W | Soil analysis | %/year | Vegetation realization | %/year | Water surface energy rate | W | Air work rate | W |
| Cloud power rate | W | Soil synthesis | %/year | Vegetation completion | %/year | Water surface energy rate | W | Air work rate | W |
| Cloud energy rate | W | Soil transformation | %/year | Vegetation attainment | %/year | Water surface energy rate | W | Air work rate | W |
| Cloud power rate | W | Soil regeneration | %/year | Vegetation achievement | %/year | Water surface energy rate | W | Air work rate | W |
| Cloud energy rate | W | Soil rejuvenation | %/year | Vegetation fulfillment | %/year | Water surface energy rate | W | Air work rate | W |
| Cloud power rate | W | Soil restoration | %/year | Vegetation completion | %/year | Water surface energy rate | W | Air work rate | W |
| Cloud energy rate | W | Soil conservation | %/year | Vegetation attainment | %/year | Water surface energy rate | W | Air work rate | W |
| Cloud power rate | W | Soil management | %/year | Vegetation achievement | %/year | Water surface energy rate | W | Air work rate | W |
| Cloud energy rate | W | Soil monitoring | %/year | Vegetation fulfillment | %/year | Water surface energy rate | W | Air work rate | W |
| Cloud power rate | W | Soil analysis | %/year | Vegetation completion | %/year | Water surface energy rate | W | Air work rate | W |
| Cloud energy rate | W | Soil synthesis | %/year | Vegetation attainment | %/year | Water surface energy rate | W | Air work rate | W |
| Cloud power rate | W | Soil transformation | %/year | Vegetation achievement | %/year | Water surface energy rate | W | Air work rate | W |
| Cloud energy rate | W | Soil regeneration | %/year | Vegetation fulfillment | %/year | Water surface energy rate | W | Air work rate | W |
| Cloud power rate | W | Soil rejuvenation | %/year | Vegetation completion | %/year | Water surface energy rate | W | Air work rate | W |
| Cloud energy rate | W | Soil restoration | %/year | Vegetation attainment | %/year | Water surface energy rate | W | Air work rate | W |
| Cloud power rate | W | Soil conservation | %/year | Vegetation achievement | %/year | Water surface energy rate | W | Air work rate | W |
| Cloud energy rate | W | Soil management | %/year | Vegetation fulfillment | %/year | Water surface energy rate | W | Air work rate | W |
| Cloud power rate | W | Soil monitoring | %/year | Vegetation completion | %/year | Water surface energy rate | | | |

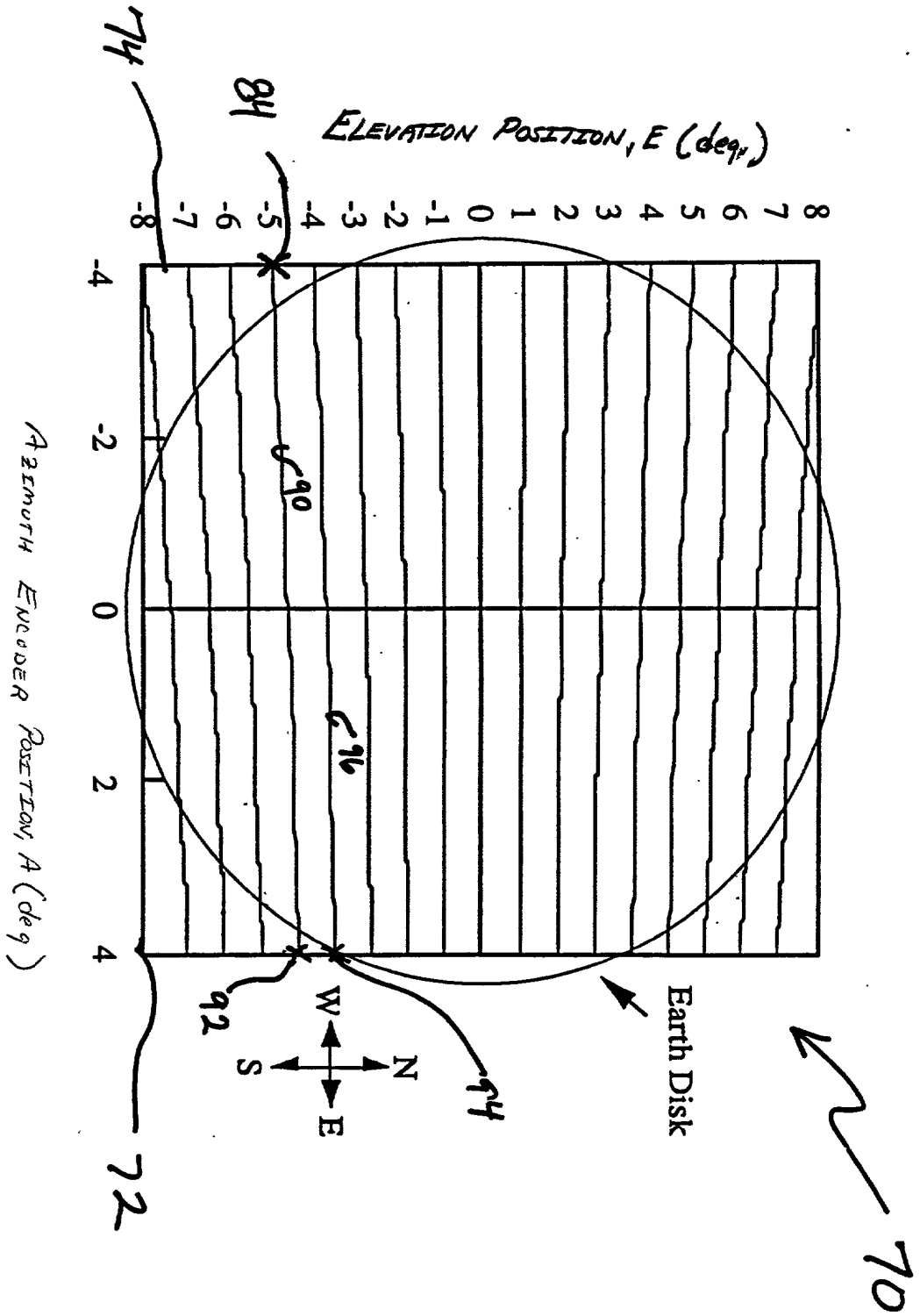
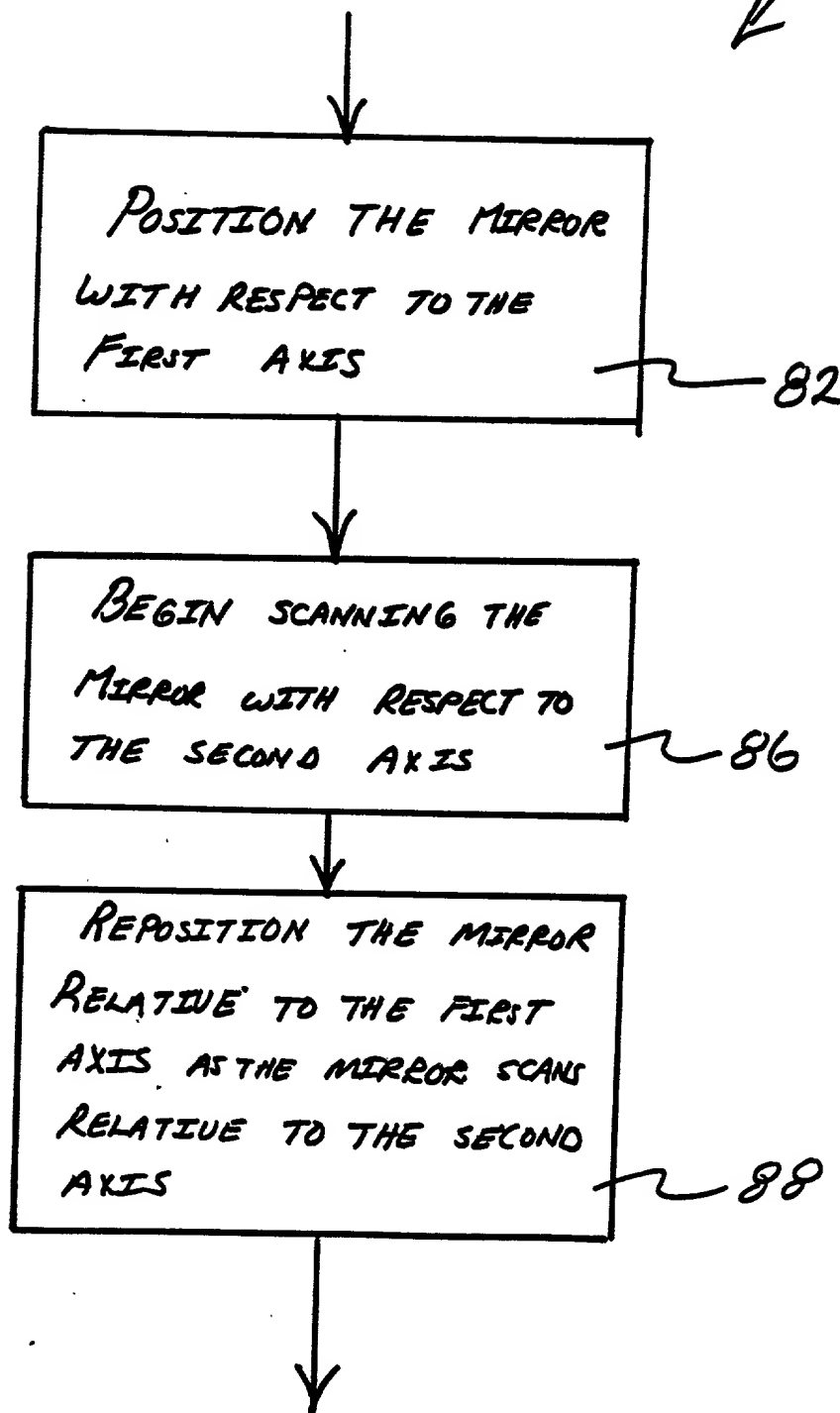


FIG. 7

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FIG. 8

MIT.8003L

DECLARATION AND POWER OF ATTORNEY

I, the below named inventor, hereby declare that:

My residence, post office address, and citizenship are as stated below next to my name.

I believe I am the original, first, and sole inventor of the subject matter which is claimed and for which a patent is sought on the invention entitled **IMAGING SYSTEM WITH A TWO-AXIS-GIMBAL MIRROR SCAN SYSTEM APPARATUS AND METHOD**, the specification of which is attached hereto

I hereby state that I have reviewed and understand the contents of the above identified specification, including the claims.

I acknowledge the duty to disclose information which is material to patentability in accordance with Title 37, Code of Federal Regulations, Section 1.56.

I hereby declare that all statements made herein based on my own knowledge are true and that all statements made on information and belief are believed to be true; and further that these statements were made with the knowledge that willful false statements and the like so made are punishable by fine or imprisonment, or both, under Section 1001 of Title 18 of the United States Code and that such willful false statements may jeopardize the validity of the application or any patent issued thereon.

And I hereby appoint:

| | |
|-----------------------|-----------------|
| Maurice E. Gauthier - | Reg. No. 20,798 |
| Richard L. Stevens - | Reg. No. 24,445 |
| Matthew E. Connors - | Reg. No. 33,298 |
| Arlene J. Powers - | Reg. No. 35,985 |
| William E. Hilton - | Reg. No. 35,192 |
| Patrick J. O'Shea - | Reg. No. 35,305 |

all of the firm of Samuels, Gauthier & Stevens, our attorneys with full power of substitution and revocation, to prosecute this application and to transact all business in the Patent and Trademark Office connected therewith.

I request that all correspondence be directed to:

Samuels, Gauthier & Stevens, LLP
225 Franklin Street, Suite 3300
Boston, Massachusetts 02110

Attn: Matthew E. Connors

Guy W. Carlisle
(Full Name of Inventor)

11-24-98
(Date)

U. S. A.
(Citizenship)

Guy W Carlisle

(Inventor's Signature)

374 Davis Road
Bedford, MA 01730
(Residence)

Same as Residence
(Post Office Address)